

# ELG4139: Oscillator Circuits

Positive Feedback Amplifiers (Oscillators)

LC and Crystal Oscillators

JBT; FET; and IC Based Oscillators

The Active-Filter-Tuned Oscillator

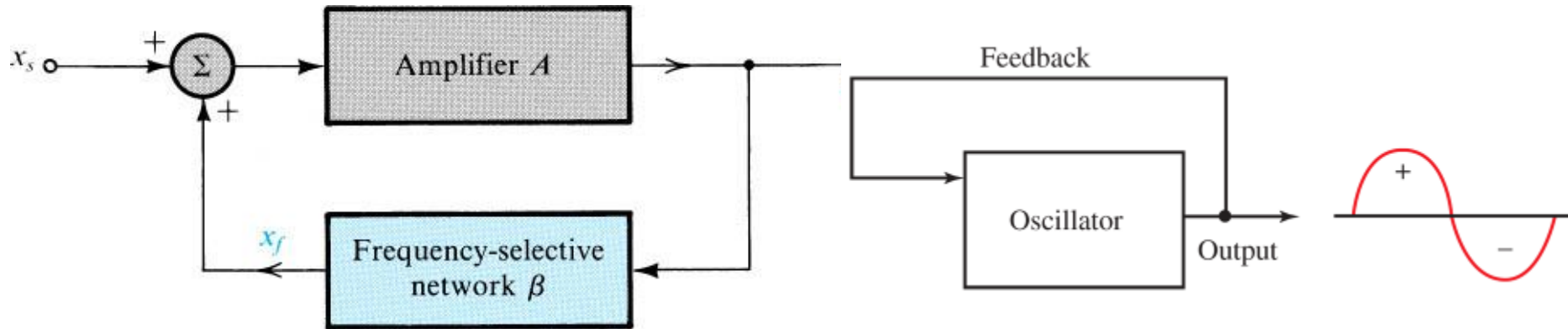
Multivibrators

# Introduction

- There are two different approaches for the generation of sinusoids, most commonly used for the standard waveforms:
  - Employing a positive-feedback loop that consists an amplifier and an RC or LC frequency-selective network. It generates sine waves utilizing resonance phenomena, are known as linear oscillators (circuits that generate square, triangular, pulse waveforms are called non-linear oscillators or function generators.)
  - A sine wave is obtained by appropriate shaping a triangular waveform.

# The Oscillator Feedback Loop

A basic structure of a sinusoidal oscillator consists of an amplifier and a frequency-selective network connected in a positive-feedback loop.



$$A_f(s) \equiv \frac{x_o}{x_i} = \frac{A(s)}{1 - A(s)\beta(s)}$$

$$L(s) \equiv A(s)\beta(s)$$

The condition for the feedback loop to provide sinusoidal oscillations of frequency  $\omega_0$  is

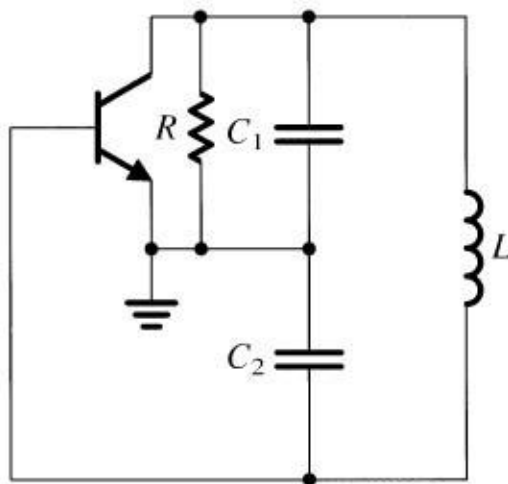
$$L(j\omega_0) \equiv A(j\omega_0)\beta(j\omega_0) = 1$$

*Barkhausen Criterion:*

- ① At  $\omega_0$  the phase of the loop gain should be zero.
- ② At  $\omega_0$  the magnitude of the loop gain should be unity.

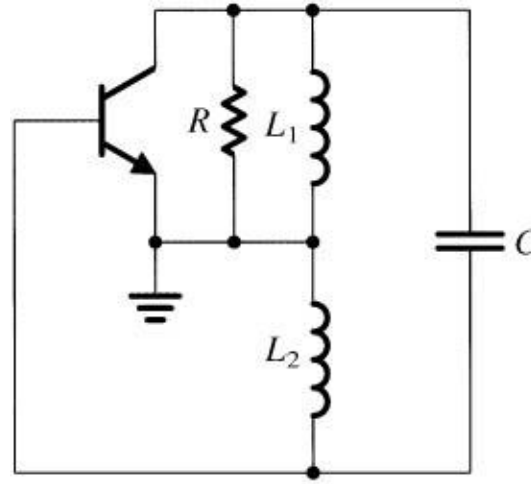
# LC and Crystal Oscillators

For higher frequencies ( $> 1\text{MHz}$ )



(a)

$$\omega_o = \frac{1}{\sqrt{L\left(\frac{C_1 C_2}{C_1 + C_2}\right)}}$$



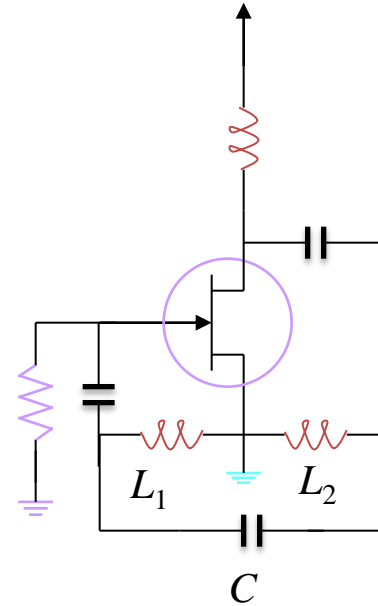
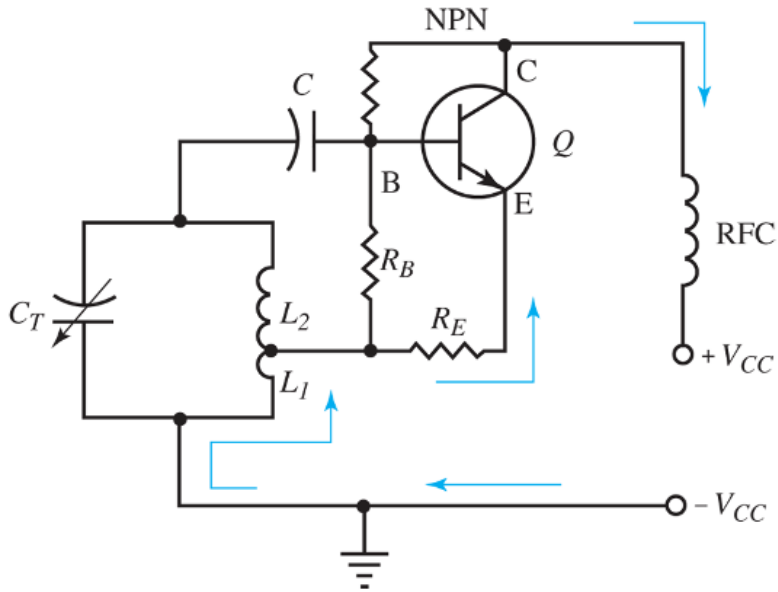
(b)

$$\omega_o = \frac{1}{\sqrt{(L_1 + L_2)C}}$$

(a) Colpitts and (b) Hartley.

# Hartley Oscillator

Used in radio receivers and transmitters More stable than Armstrong oscillators Radio frequency choke (RFC)

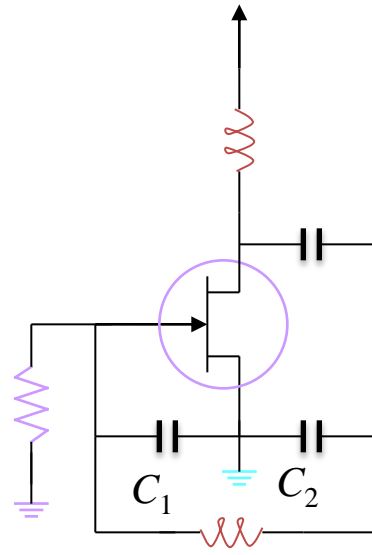
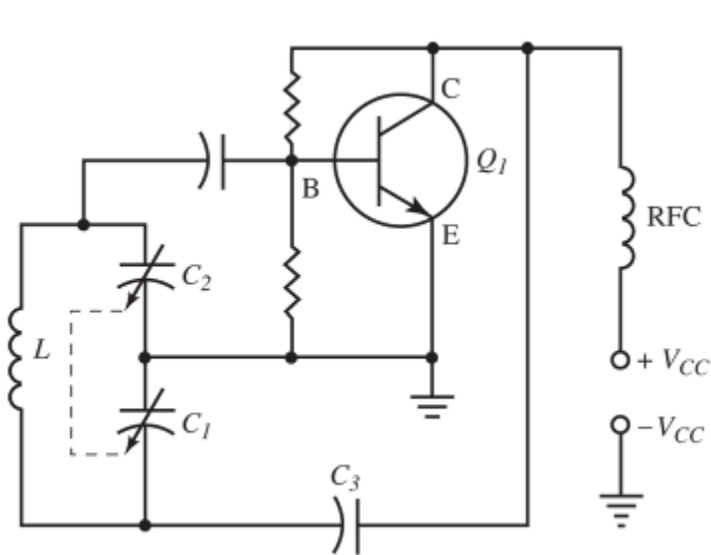


$$f_0 = \frac{1}{2\pi\sqrt{L_{eq}C}} \quad \text{where } L_{eq} = L_1 + L_2 + 2M$$

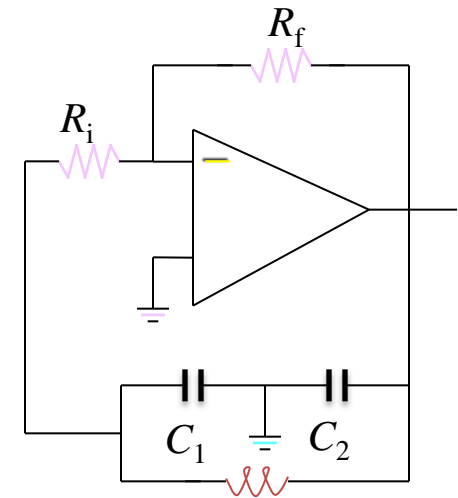
$M = \text{Mutual coupling between } L_1 \text{ \& } L_2$

# Colpitts Oscillators

## BJT; FET; and IC Based



LC network

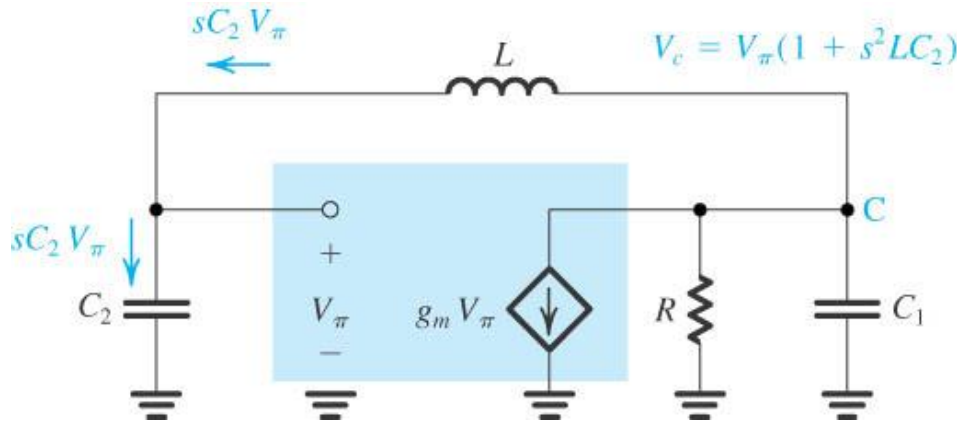


LC network

$$f_0 = \frac{1}{2\pi\sqrt{LC_{eq}}} \quad \text{where } C_{eq} = \frac{C_1 C_2}{C_1 + C_2}$$

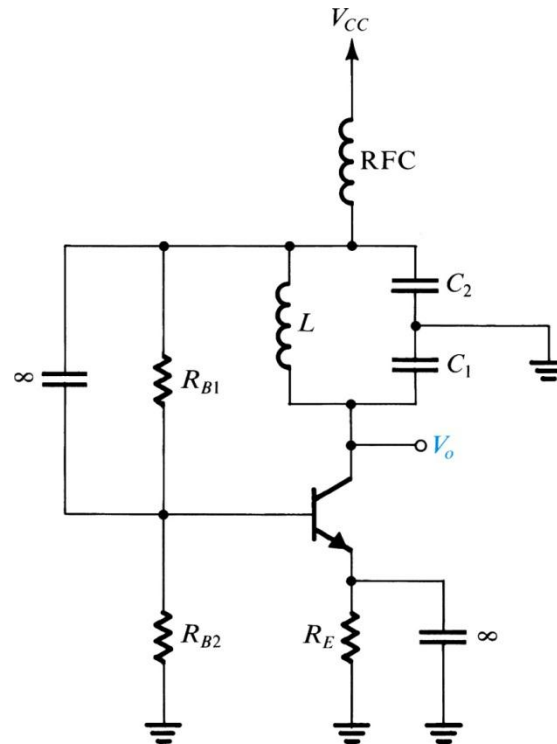
RFC is an impedance which is high (open) at high RF frequencies and low (short) to dc voltages

# Equivalent Circuit of the Colpitts Oscillator



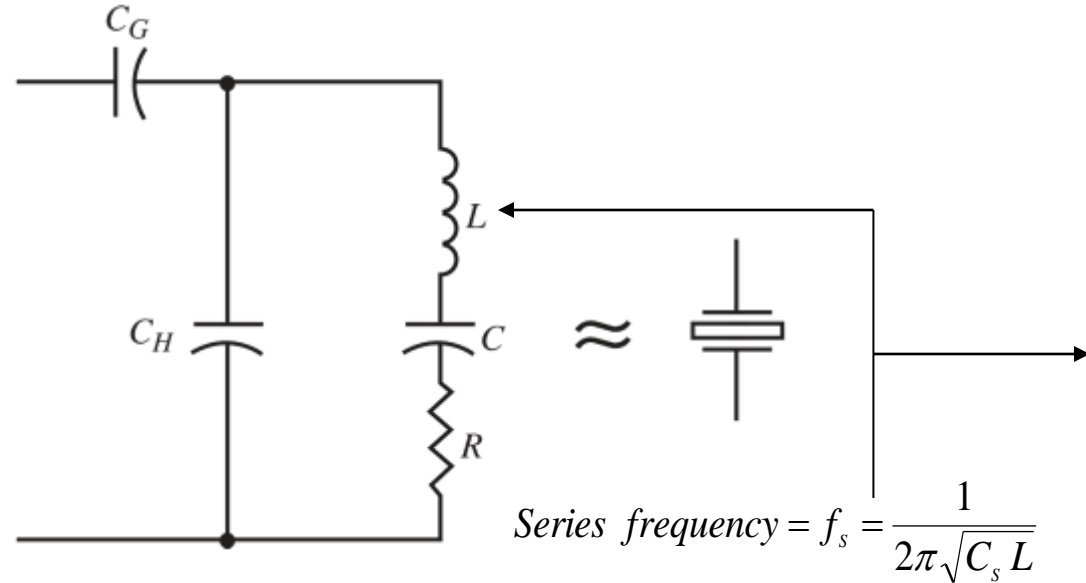
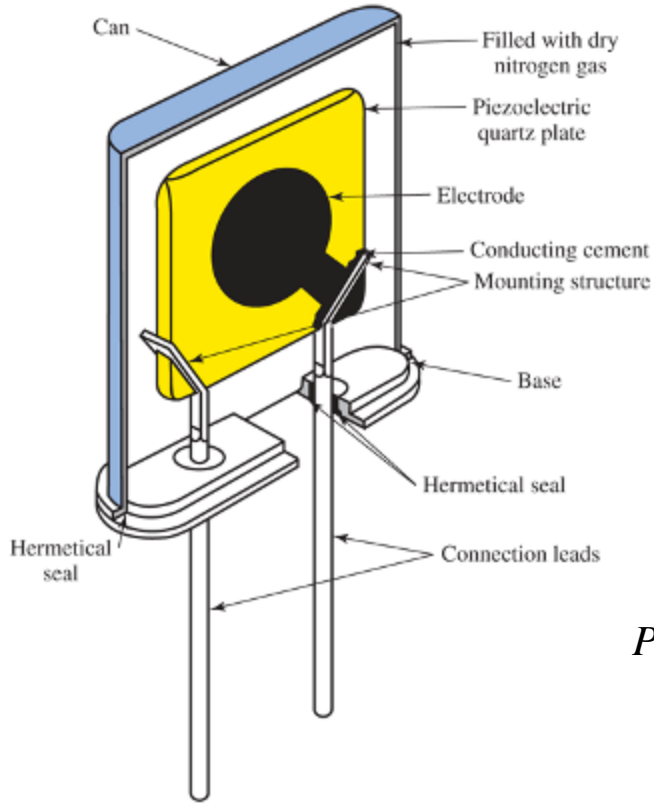
$$\omega_0 = \frac{1}{\sqrt{L \left( \frac{C_1 C_2}{C_1 + C_2} \right)}}$$

# Complete Circuit for a Colpitts Oscillator



# Crystal Oscillators

Crystal is a piezo-electric device which converts mechanical pressure to electrical voltage or vice-versa



$$\text{Parallel frequency} = f_p = \frac{1}{2\pi\sqrt{\left(\frac{C_s C_p}{C_s + C_p}\right) L}}$$

Radio communications, broadcasting stations

Piezoelectric effect

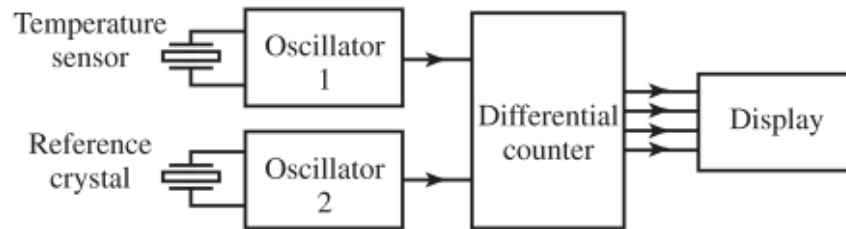
Why are crystal oscillators used in many commercial transmitters?



# An Application of Crystal Oscillator

Crystals are fabricated by cutting the crude quartz in a very exacting fashion. The type of cut determines the crystal's natural resonant frequency as well as its temperature coefficient.

Crystals are available at frequencies about 15kHz and up providing the best frequency stability. However above 100MHz, they become so small that handling becomes a problem.



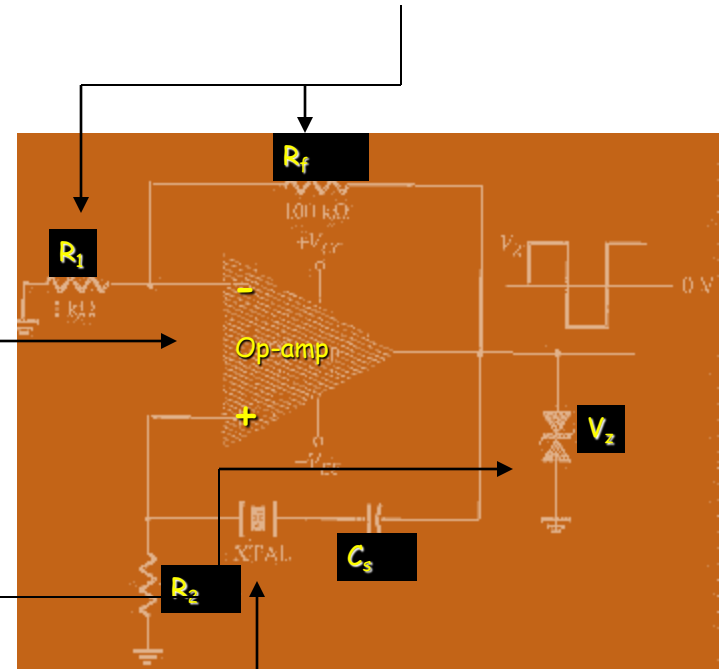
Two crystals producing two different frequencies for measuring temperature Timing devices

# Op-Amp Crystal Oscillator

Op-amp voltage gain is controlled by the negative feedback circuit formed by  $R_f$  and  $R_1$ . More NFB will damp the oscillation, critical NFB will have a sine wave output and less NFB will have a square wave output.

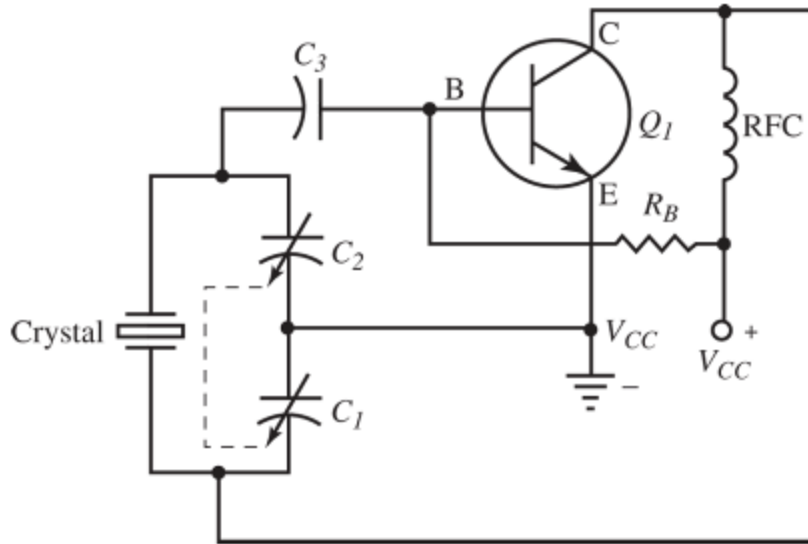
It is very flexible to construct the Op. Amp. crystal oscillator due to high amplifier gain and differential input facility of the Op. Amp.

The two Zener diodes connected face to face is to limit the peak to peak output voltage equal to twice of Zener voltage.



The crystal is fed in series to the positive feedback which is required for oscillation. Therefore the oscillation frequency will be crystal series resonant frequency  $f_s$ .

# Example



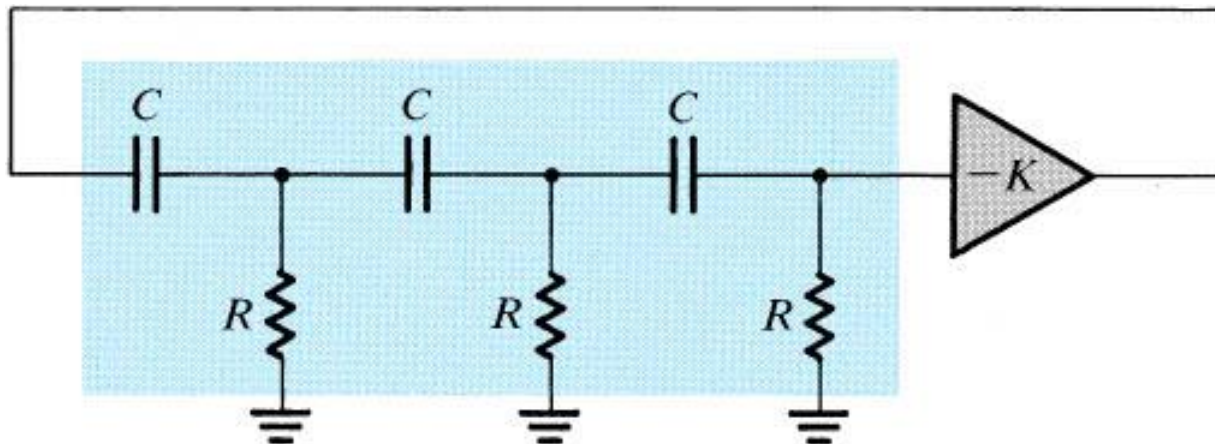
Crystal used instead of inductor in the tank circuit of Colpitts oscillator

# The Phase Shifter Oscillator

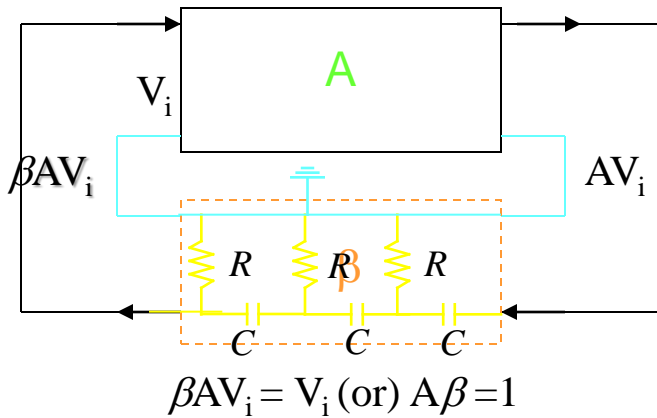
The phase-shifter consists of a negative gain amplifier ( $-K$ ) with a third order RC ladder network in the feedback.

The circuit will oscillate at the frequency for which the phase shift of the RC network is  $180^\circ$ . Only at the frequency will the total phase shift around the loop be  $0^\circ$  or  $360^\circ$ .

The minimum number of RC sections is 3 because it is capable of producing a  $180^\circ$  phase shift at a finite frequency.



# Phase-shift Oscillator



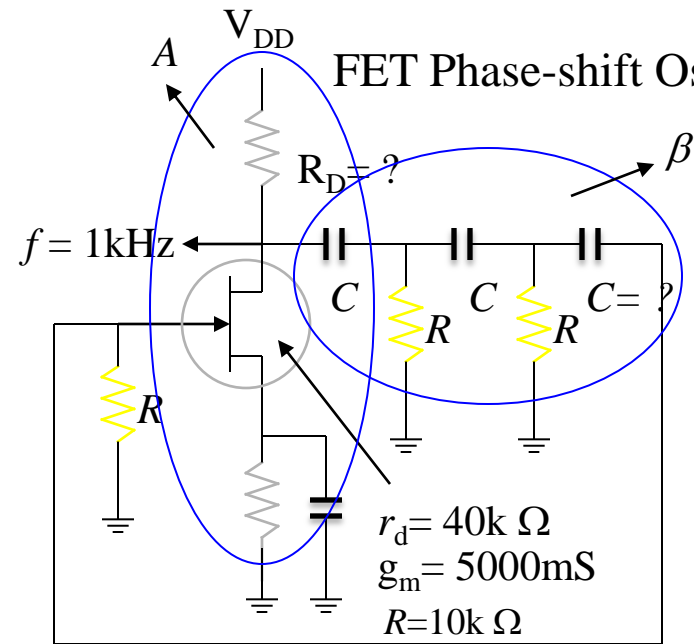
Frequency of oscillation

$$f = \frac{1}{2\pi RC \sqrt{6}}$$

Condition of oscillation

$$\beta \leq \frac{1}{29} \quad A\beta = 1 \quad \therefore A \geq 29$$

# FET Phase-shift Oscillator



## Example:

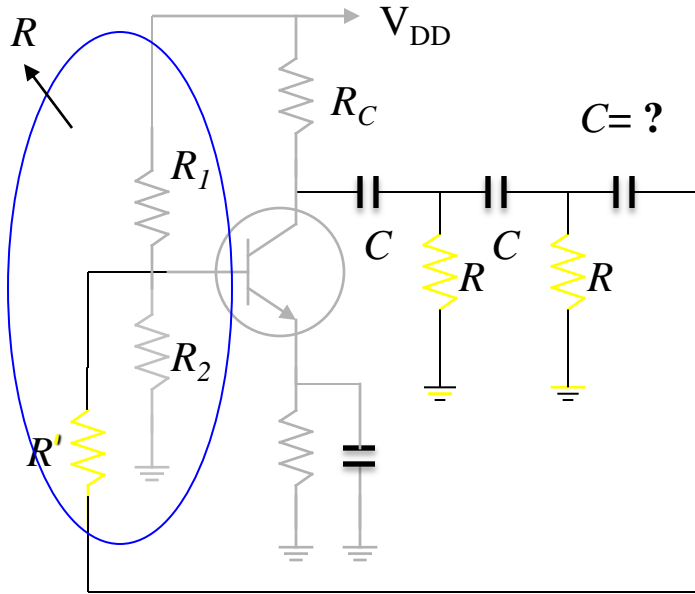
Determine the value of capacitance  $C$  and the value of  $R_D$  of the Phase-shift oscillator shown, if the output frequency is 1 kHz. Take  $r_d = 40k$  and  $g_m = 5000mS$ , for the FET and  $R = 10k\Omega$ .

$$f = \frac{1}{2\pi RC \sqrt{6}} \Rightarrow C = \frac{1}{2\pi R f \sqrt{6}} = \frac{1}{2\pi 10k \times 1k \sqrt{6}} = \underline{\underline{6.5nF}}$$

$$A\beta \geq 1 \quad \text{Let } A = 40 > 29 \therefore |A| = g_m R_L = 40 \Rightarrow R_L = \frac{40}{g_m} = \frac{40}{5000\mu S} = 8k\Omega$$

$$\text{But } R_L = R_D // r_d = R_D // 40k\Omega = 8k\Omega \therefore R_D = \frac{8k \times 40k}{40k - 8k} = \underline{\underline{10k\Omega}}$$

# BJT Phase-Shift Oscillator



## Example:

Determine the value of capacitance  $C$  and the value of  $h_{fe}$  of the Phase-shift oscillator shown, if the output frequency is 1kHz.

Take  $R=10\text{ k}$ .  $R_C=1\text{ k}$ .

$$f = \frac{1}{2\pi RC\sqrt{6 + 4R_C/R}} = 1\text{kHz} = \frac{1}{2\pi 10\text{k}C\sqrt{6 + 4 \times 1\text{k}/10\text{k}}}$$

$$C = \frac{1}{2\pi 10\text{k} \times 1\text{k} \sqrt{6 + 4 \times 1\text{k}/10\text{k}}} = 0.006\mu\text{F} = \underline{\underline{6\text{nF}}}$$

Frequency of oscillation

$$f = \frac{1}{2\pi RC\sqrt{6 + 4R_C/R}}$$

Condition of oscillation

$$A\beta = 1 \Rightarrow \therefore A \geq 29$$

$$\beta \leq \frac{1}{29}$$

$$\text{for BJT} \Rightarrow h_{fe} \geq 23 + 29 \frac{R}{R_C} + 4 \frac{R_C}{R}$$

$$\text{for BJT} \Rightarrow h_{fe} \geq 23 + 29 \frac{R}{R_C} + 4 \frac{R_C}{R}$$

$$\geq 23 + 29 \frac{10\text{k}}{1\text{k}} + 4 \frac{1\text{k}}{10\text{k}} \geq 23 + 290 + 0.4 \geq \underline{\underline{313.4}}$$

# IC Phase-shift Oscillator

Frequency of oscillation

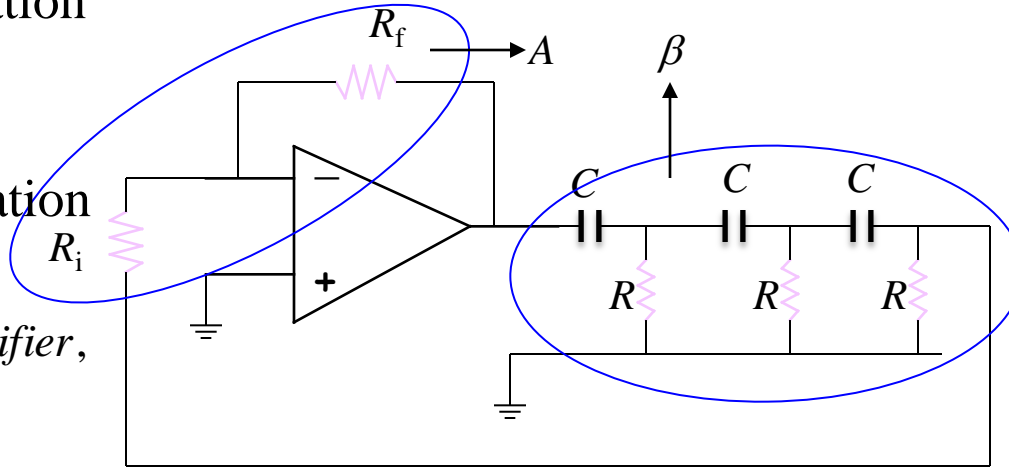
$$f = \frac{1}{2\pi RC\sqrt{6}}$$

Condition of oscillation

$$A\beta = 1 \therefore A \geq 29$$

for IC inverting amplifier,

$$|A| = \frac{R_f}{R_i} \geq 29 \quad \beta \leq \frac{1}{29}$$



## Example:

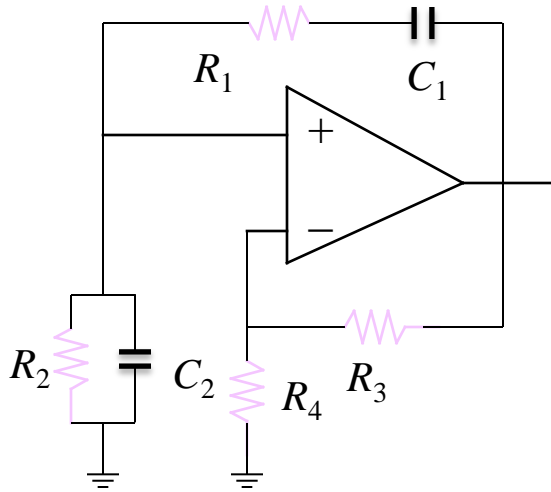
Determine the value of capacitance  $C$  and the value of  $R_f$  of the IC Phase-shift oscillator shown, if the output frequency is 1kHz. Take  $R = 10\text{k}\Omega$ .  $R_i = 1\text{k}\Omega$ .

$$f = \frac{1}{2\pi RC\sqrt{6}} \Rightarrow C = \frac{1}{2\pi Rf\sqrt{6}} = \frac{1}{2\pi 10\text{k} \times 1\text{k}\sqrt{6}} = \underline{\underline{6.5\text{nF}}}$$

for IC inverting amplifier,

$$|A| = \frac{R_f}{R_i} \geq 29 \Rightarrow R_f \geq 29R_i \geq \underline{\underline{29\text{k}\Omega}}$$

# Wien Bridge Oscillator



Frequency of oscillation

$$f = \frac{1}{2\pi\sqrt{R_1 C_1 R_2 C_2}} \quad f = \frac{1}{2\pi RC} \left( \begin{array}{l} \text{if } R_1 = R_2 = R \\ C_1 = C_2 = C \end{array} \right)$$

Condition of oscillation

$$\frac{R_3}{R_4} = \frac{R_1}{R_2} + \frac{C_2}{C_1} \quad \frac{R_3}{R_4} = 2 \left( \begin{array}{l} \text{if } R_1 = R_2 = R \\ C_1 = C_2 = C \end{array} \right)$$

**Example:** Determine the value of capacitance  $C_1$  and  $R_1$  if  $R_2 = 10k\Omega$   $C_2 = 0.1\mu F$   $R_3 = 10k\Omega$   $R_4 = 1k\Omega$  in the Wien bridge oscillator shown has an output frequency of 1kHz.

$$f = \frac{1}{2\pi\sqrt{R_1 C_1 R_2 C_2}} \Rightarrow f^2 = \frac{1}{4\pi^2 R_1 C_1 R_2 C_2} \quad \text{Frequency of oscillation}$$

$$R_1 C_1 = \frac{1}{4\pi^2 f^2 R_2 C_2} = \frac{1}{4\pi^2 (1k)^2 10k \times 0.1\mu} = 0.025ms \Rightarrow C_1 = \frac{0.025ms}{R_1}$$

$$\frac{R_3}{R_4} = \frac{R_1}{R_2} + \frac{C_2}{C_1} \Rightarrow \frac{10k}{1k} = \frac{R_1}{10k} + \frac{0.1\mu F}{0.025ms} \Rightarrow \frac{R_1}{10k} = 10 - \frac{0.1}{25} = 9.996$$

$$R_1 = 9.996 \times 10k = 99.96k \approx \underline{\underline{100k\Omega}}$$

$$C_1 = \frac{0.025ms}{100k} = 0.00025\mu = \underline{\underline{250pF}}$$

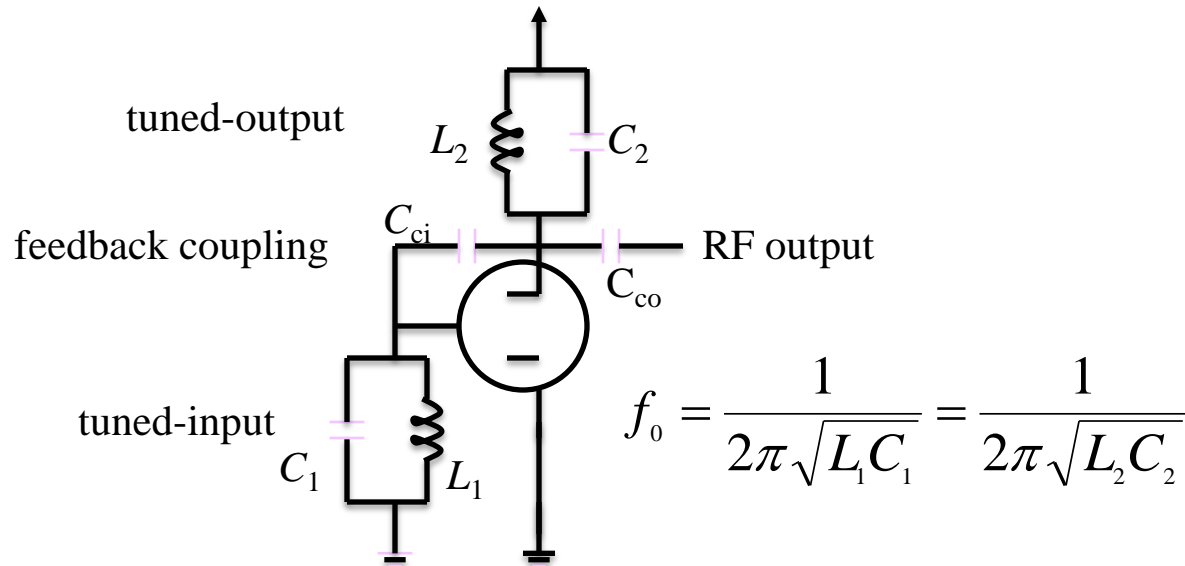
Condition of oscillation



# Tuned Oscillators (Radio Frequency Oscillators)

Tuned oscillator is a circuit that generates a radio frequency output by using LC tuned (resonant) circuit. Because of high frequencies, small inductance can be used for the radio frequency of oscillation.

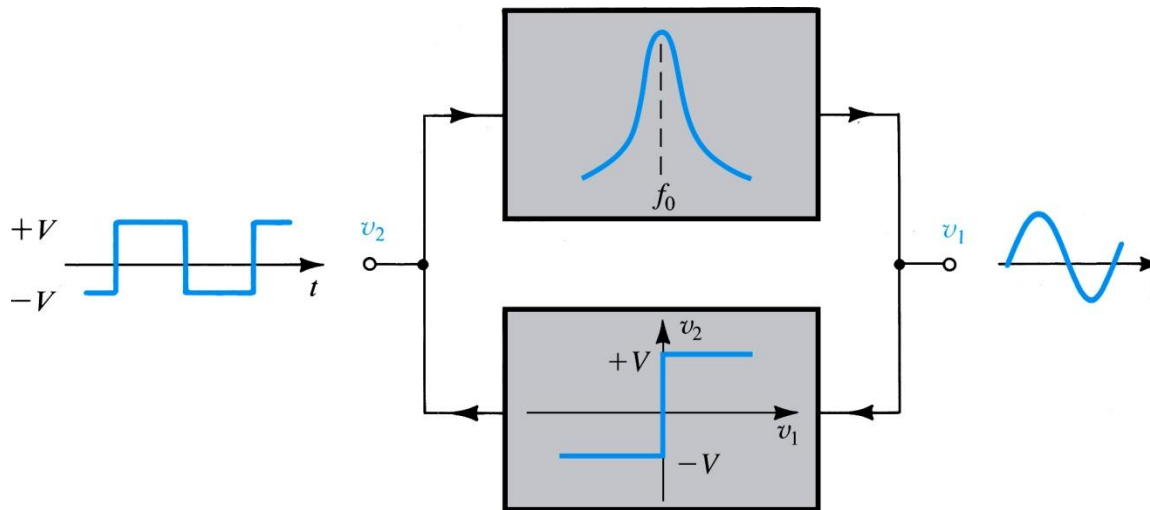
Tuned-input and tuned-output Oscillator

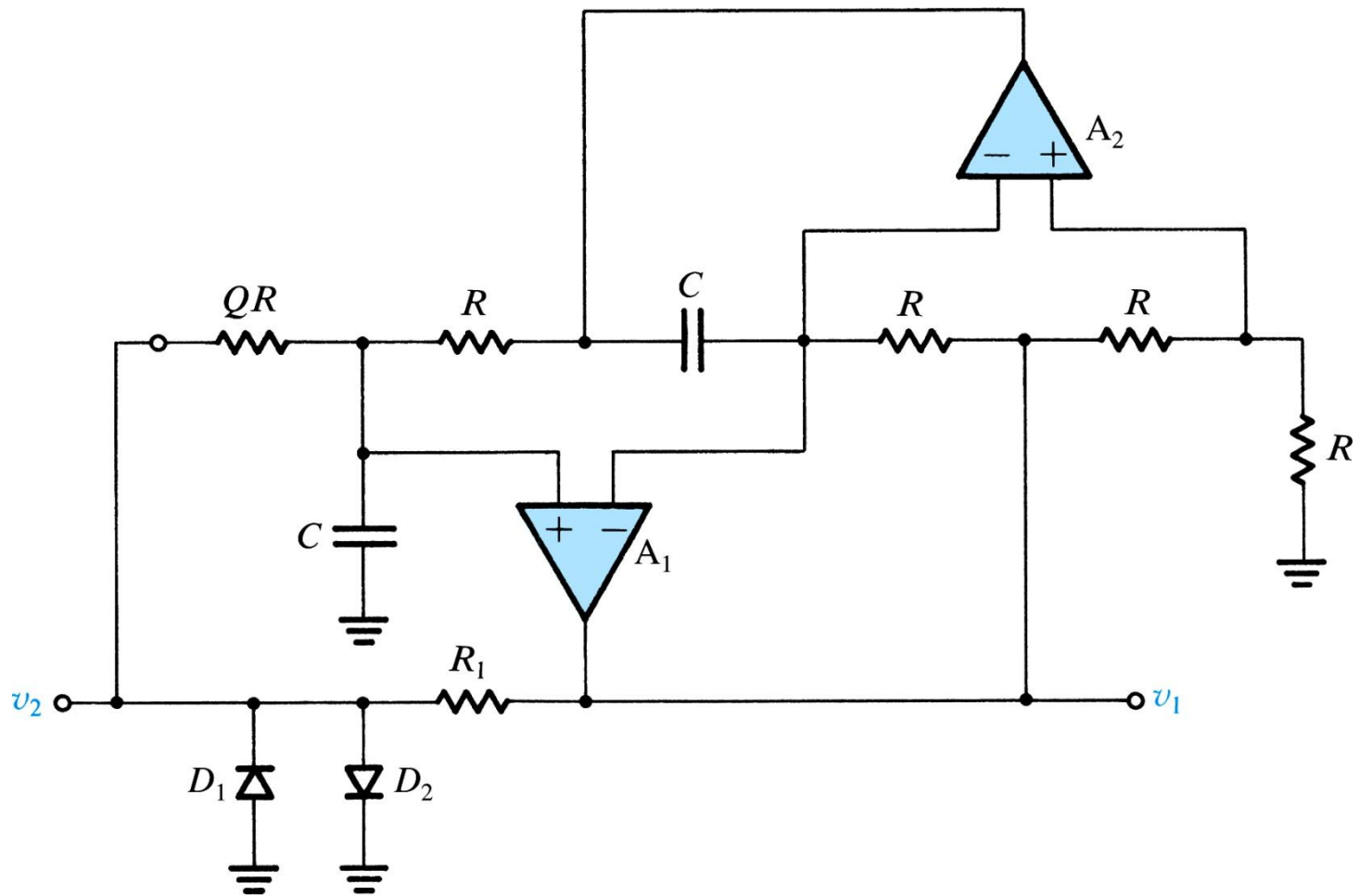


# The Active-Filter-Tuned Oscillator

Assume the oscillations have already started. The output of the band-pass filter will be a sine wave whose frequency is equal to the center frequency of the filter.

The sine-wave signal is fed to the limiter and then produces a square wave.



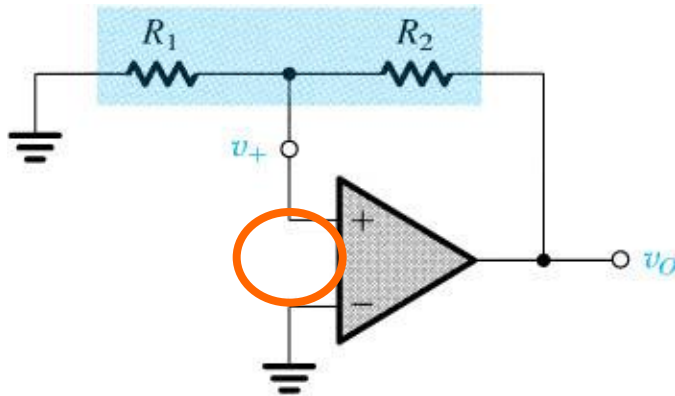


Practical implementation of the active-filter-tuned oscillator

# Bistable Multivibrators

Another type of waveform generating circuits is the nonlinear oscillators or function generators which uses multivibrators.

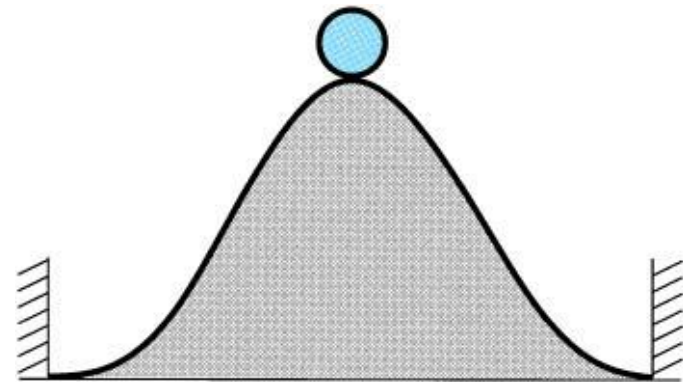
A **bistable** multivibrator has **2 stable states**. The circuit can remain in either state indefinitely and changes to the other one only when **triggered**.

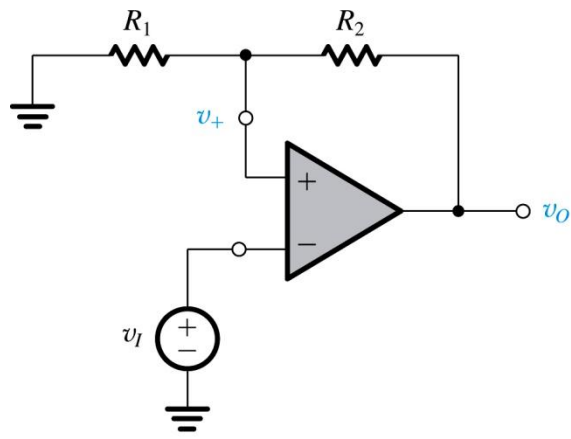


Metastable state:  $v_+ = 0$  and  $v_O = 0$ . The circuit cannot exist in the metastable state for any length of time since any disturbance causes it to switch to either stable state.

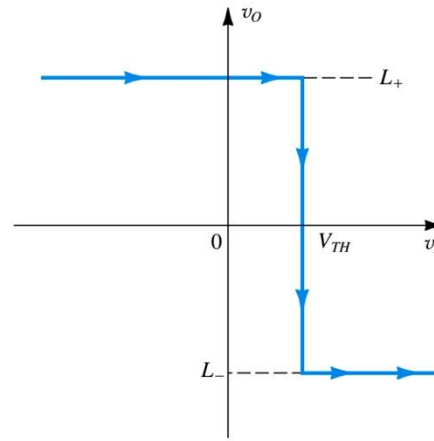
$$v_O = L_+ \text{ and } v_+ = L_+ R_1 / (R_1 + R_2).$$

$$v_O = L_- \text{ and } v_+ = L_- R_1 / (R_1 + R_2).$$

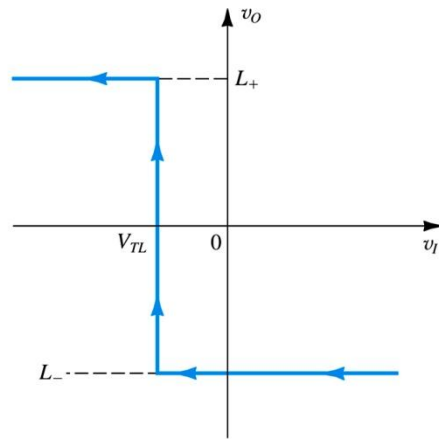




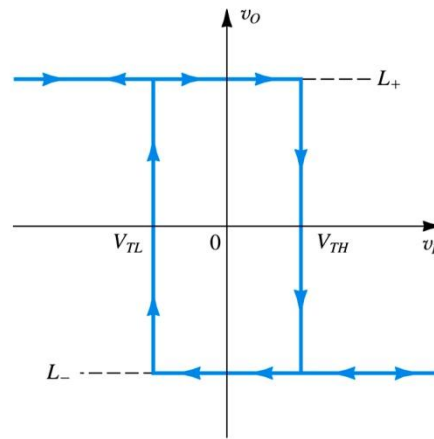
(a)



(b)



(c)



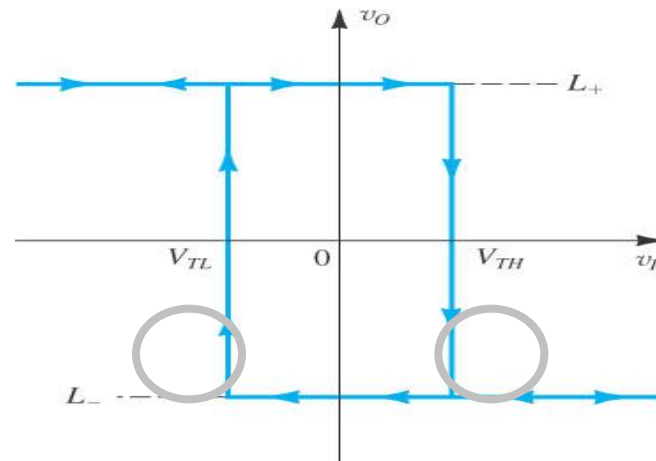
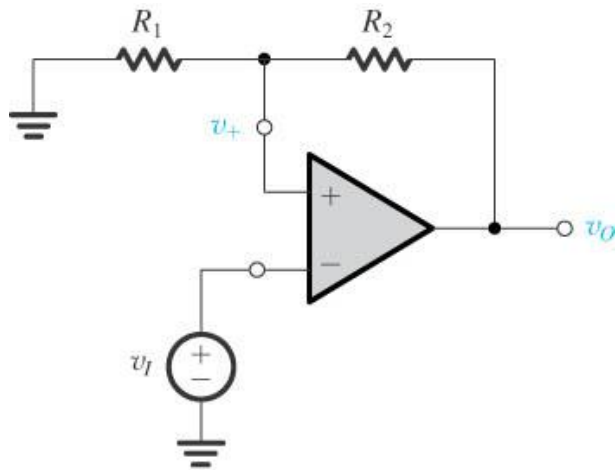
(d)

**Figure 12.19** (a) The bistable circuit of Fig. 12.17 with the negative input terminal of the op amp disconnected from ground and connected to an input signal  $v_I$ . (b) The transfer characteristic of the circuit in (a) for increasing  $v_I$ . (c) The transfer characteristic for decreasing  $v_I$ . (d) The complete transfer characteristics.

# Bistable Circuit with Inverting Transfer Characteristics

Assume that  $v_O$  is at one of its two possible levels, say  $L_+$ , and thus  $v_+ = \beta L_+$ .

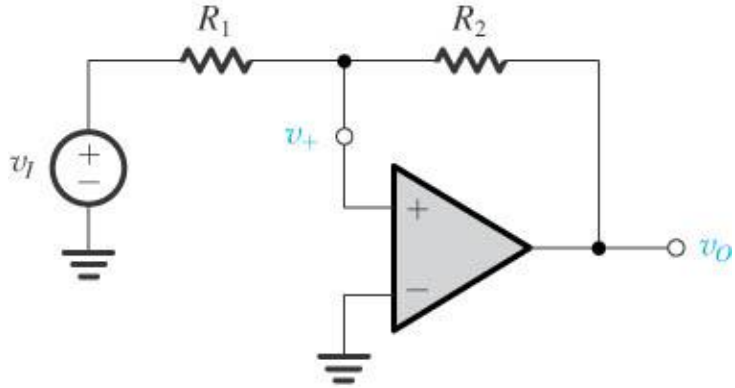
- ① As  $v_I$  increases from 0 and then exceeds  $\beta L_+$ , a negative voltage develops between input terminals of the op amp.
- ② This voltage is amplified and  $v_O$  goes negative.
- ③ The voltage divider causes  $v_+$  to go negative, increasing the net negative input and keeping the regenerative process going.
- ④ This process culminates in the op amp saturating, that is,  $v_O = L_-$ .



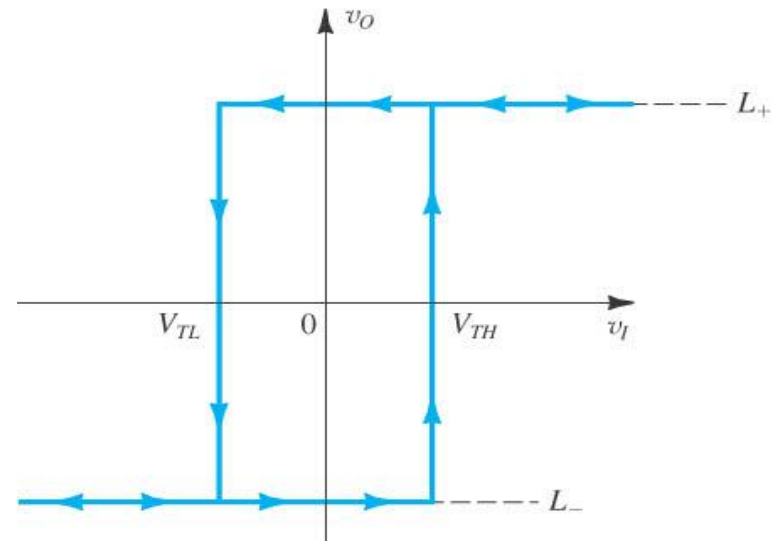
The circuit is said to be inverting

Trigger signal

# Bistable Circuit with Noninverting Transfer Characteristics

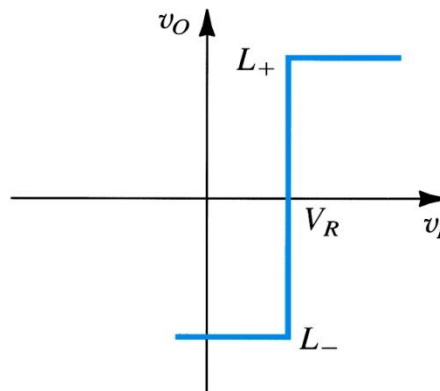
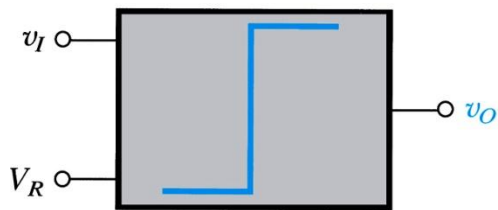


$$v_+ = v_I R_2 / (R_1 + R_2) + v_O R_1 / (R_1 + R_2)$$

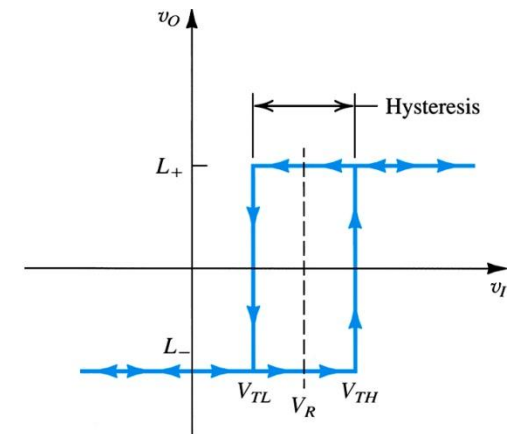


$$V_{TL} = -L_+(R_1/R_2)$$

$$V_{TH} = -L_-(R_1/R_2)$$



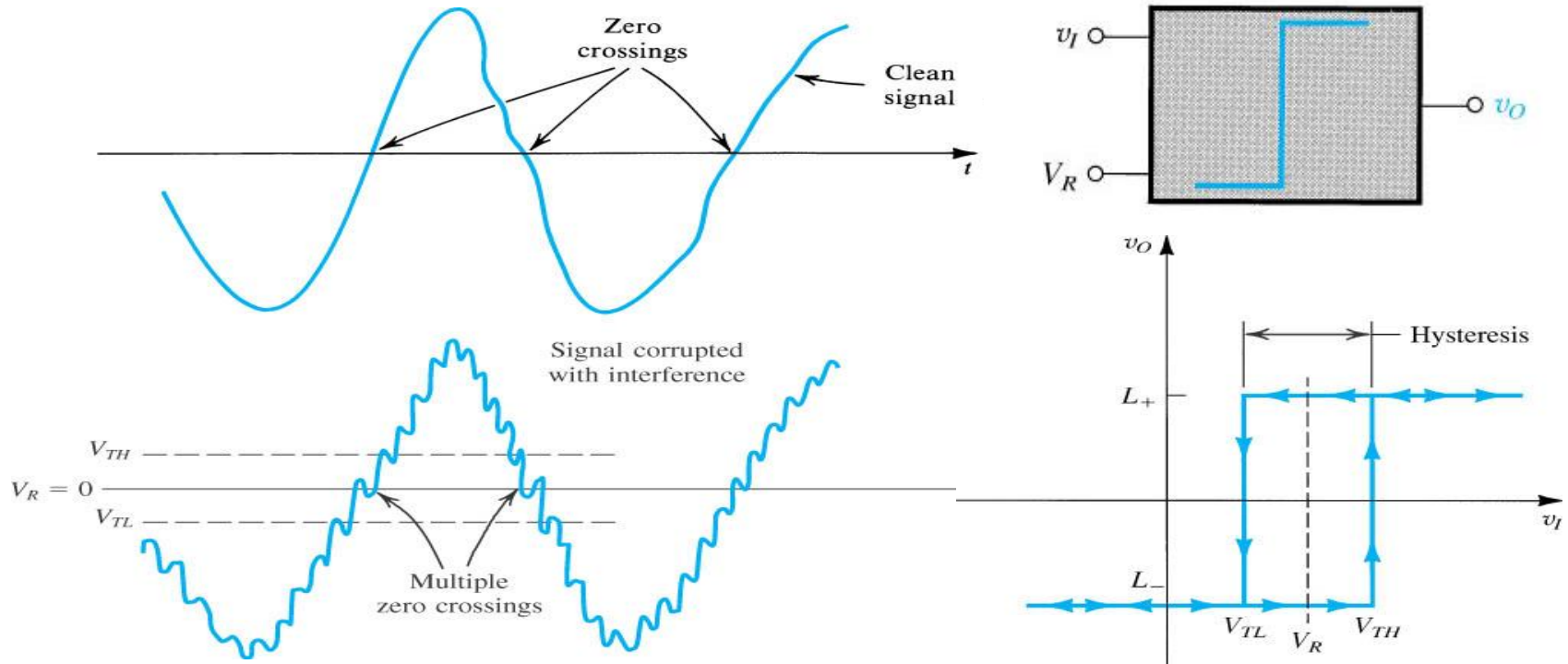
(a)



(b)

# Application of the Bistable Circuit as a Comparator

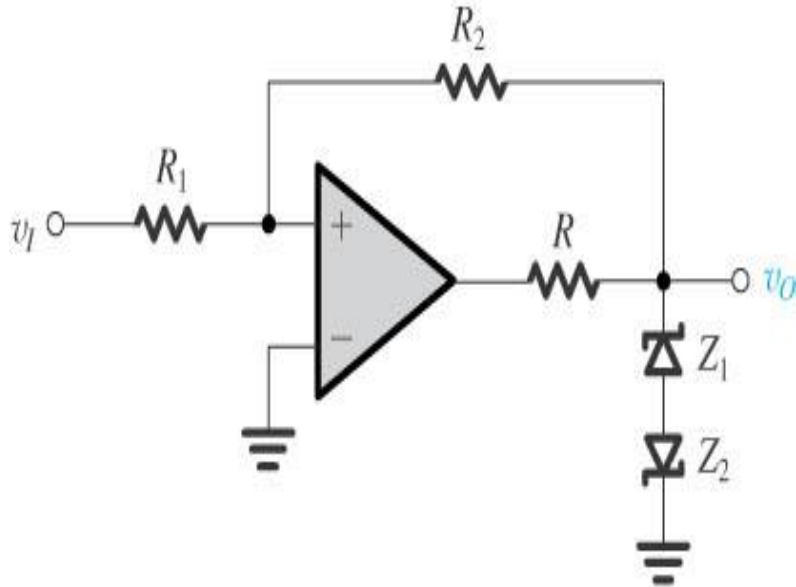
To design a circuit that detects and counts the zero crossings of an arbitrary waveform, a comparator whose threshold is set to 0 can be used. The comparator provides a step change at its output every time zero crossing occurs.





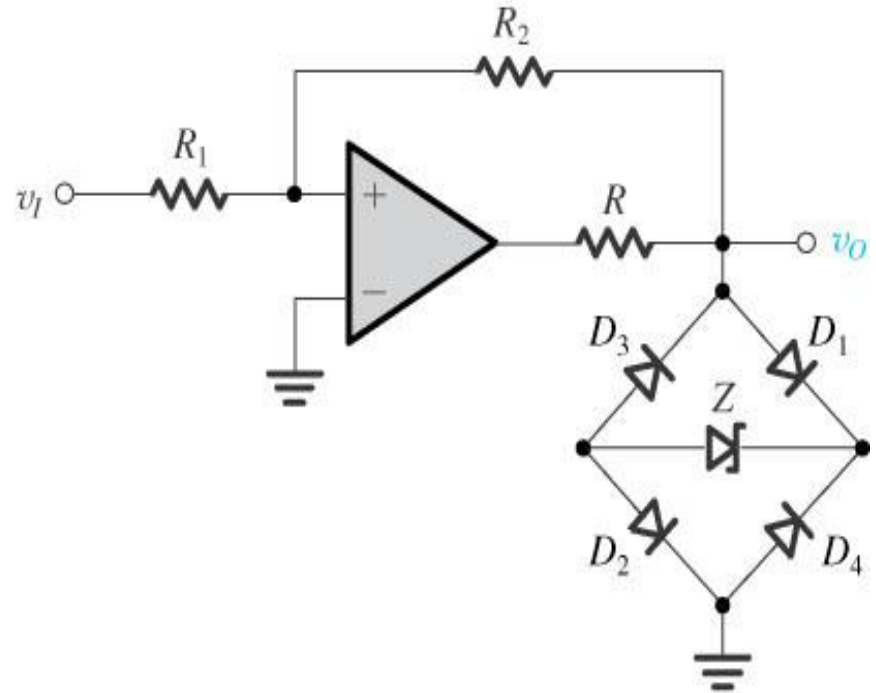
# Bistable Circuit with More Precise Output Level

Limiter circuits are used to obtain more precise output levels for the bistable circuit.



$$L_+ = V_{Z1} + V_D \text{ and } L_- = -(V_{Z2} + V_D),$$

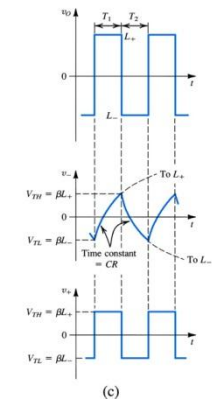
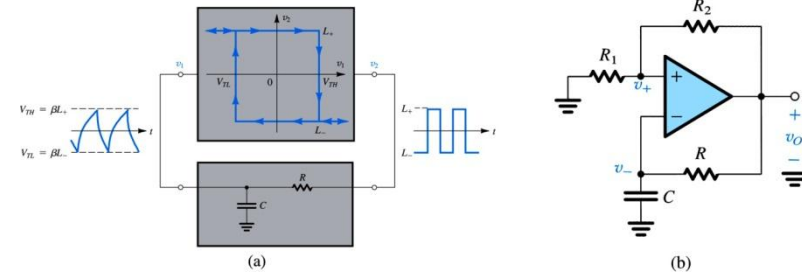
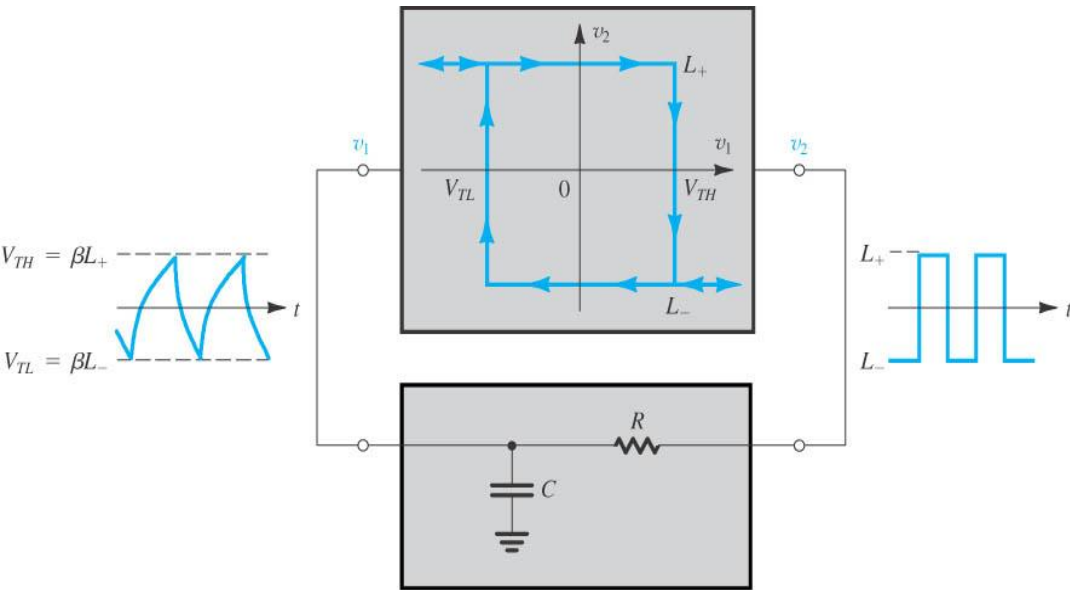
where  $V_D$  is the forward diode drop.



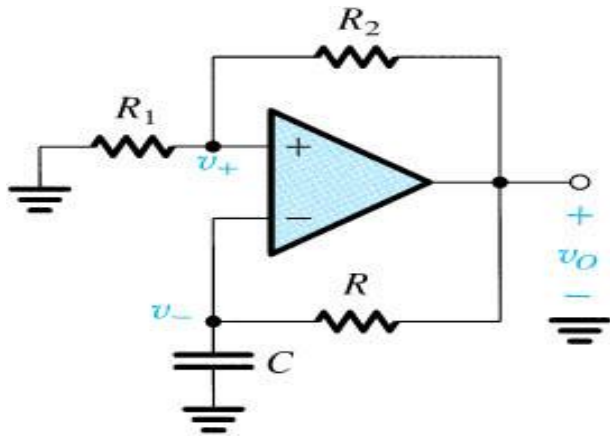
$$L_+ = V_Z + V_{D1} + V_{D2} \text{ and } L_- = -(V_Z + V_{D3} + V_{D4}).$$

# Operation of the Astable Multivibrator

Connecting a bistable multivibrator with inverting transfer characteristics in a feedback loop with an RC circuit results in a square-wave generator.



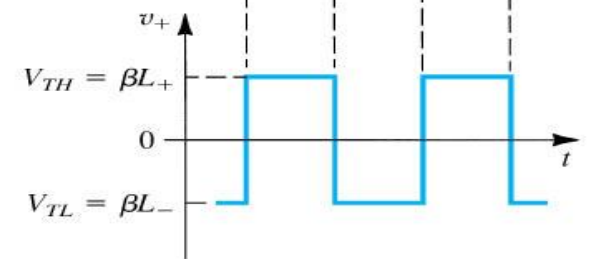
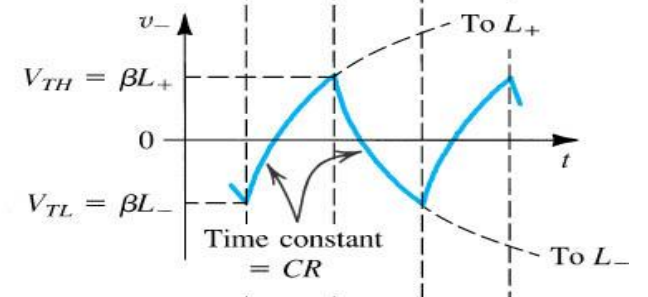
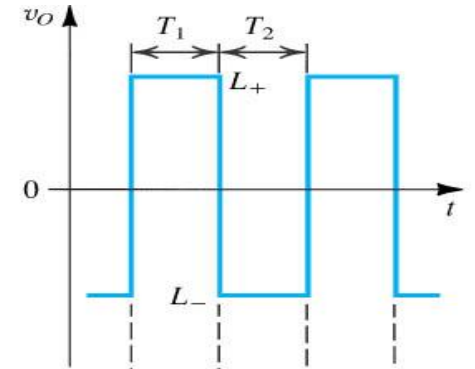
# Operation of the Astable Multivibrator



$$v_- = L_+ - (L_+ - \beta \cdot L_-)e^{-T_1/RC} = \beta \cdot L_+ \quad \rightarrow T_1 = \tau \ln \frac{1 - \beta(L_- / L_+)}{1 - \beta}$$

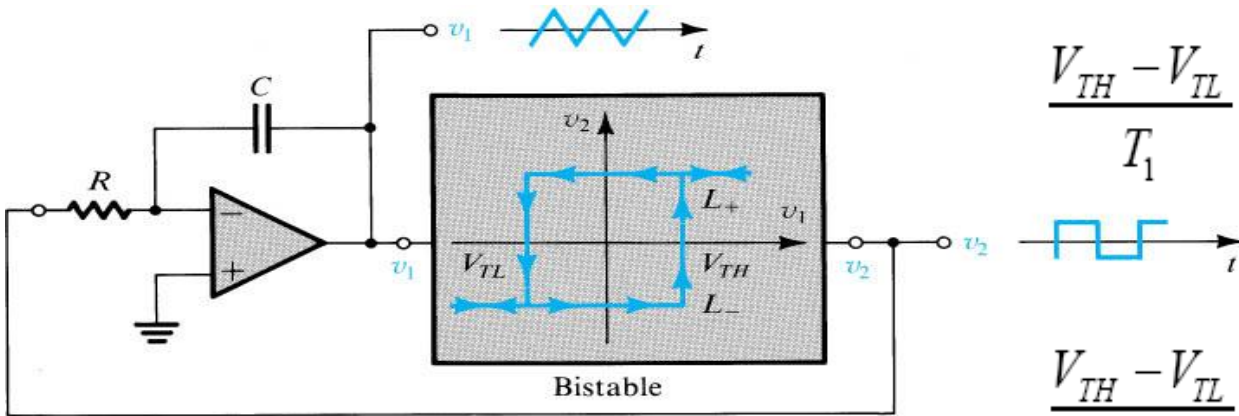
$$v_- = L_- - (L_- - \beta \cdot L_+)e^{-T_2/RC} = \beta L_- \quad \rightarrow T_2 = \tau \ln \frac{1 - \beta(L_+ / L_-)}{1 - \beta}$$

$$T \approx 2\tau \ln \frac{1 + \beta}{1 - \beta}$$



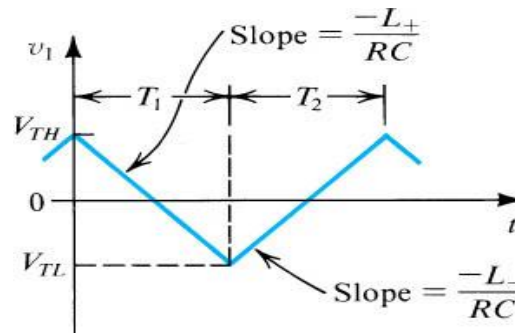
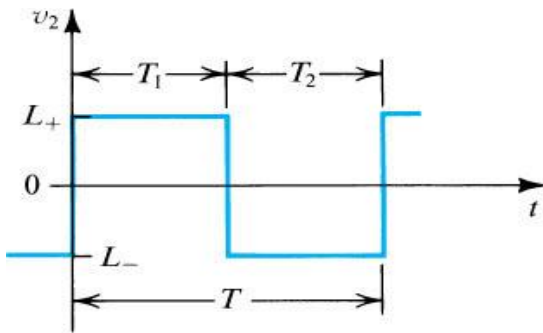
# Generation of Triangular Waveforms

Triangular waveforms can be obtained by replacing the low-pass RC circuit with an integrator. Since the integrator is inverting, the inverting characteristics of the bistable circuit is required.



$$\frac{V_{TH} - V_{TL}}{T_1} = \frac{L_+}{RC} \rightarrow T_1 = RC \frac{V_{TH} - V_{TL}}{L_+}$$

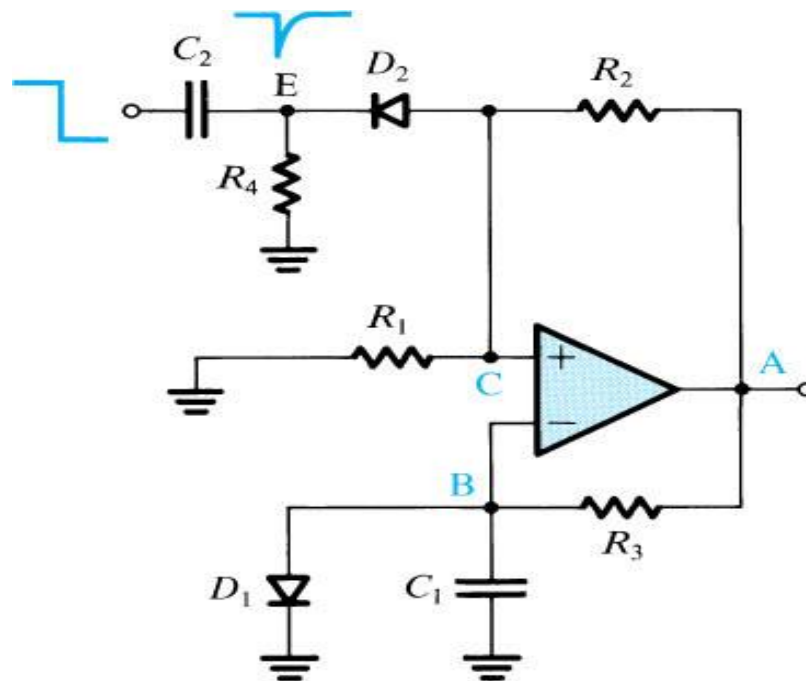
$$\frac{V_{TH} - V_{TL}}{T_2} = \frac{-L_-}{RC} \rightarrow T_2 = RC \frac{V_{TH} - V_{TL}}{-L_-}$$



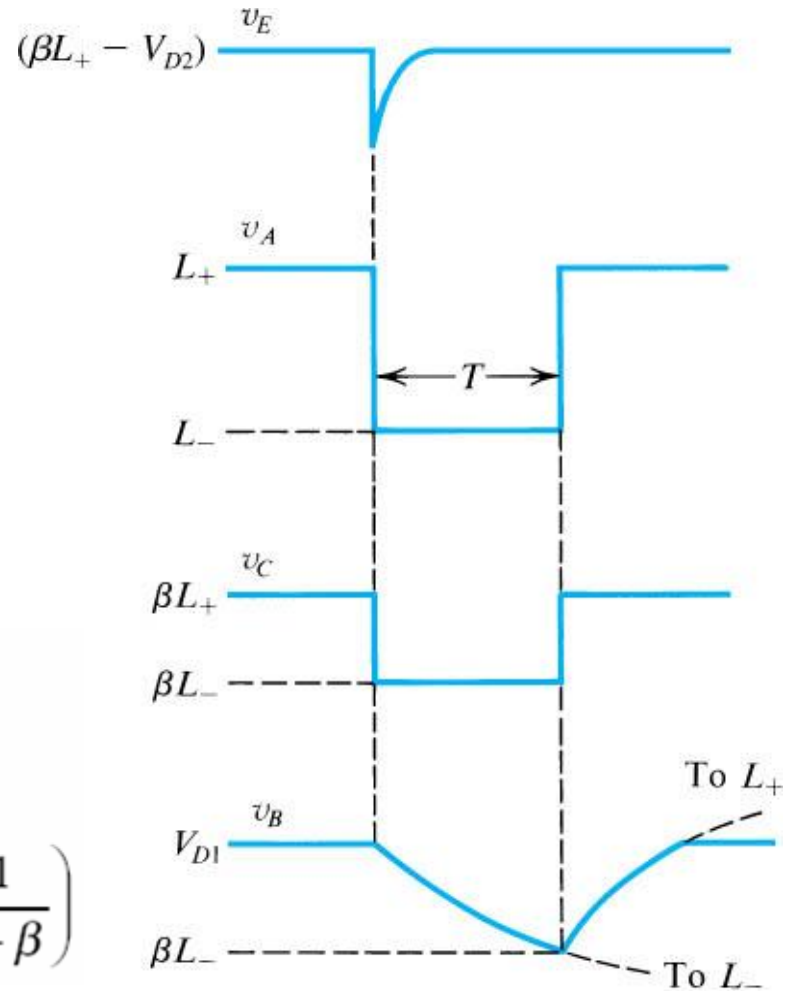
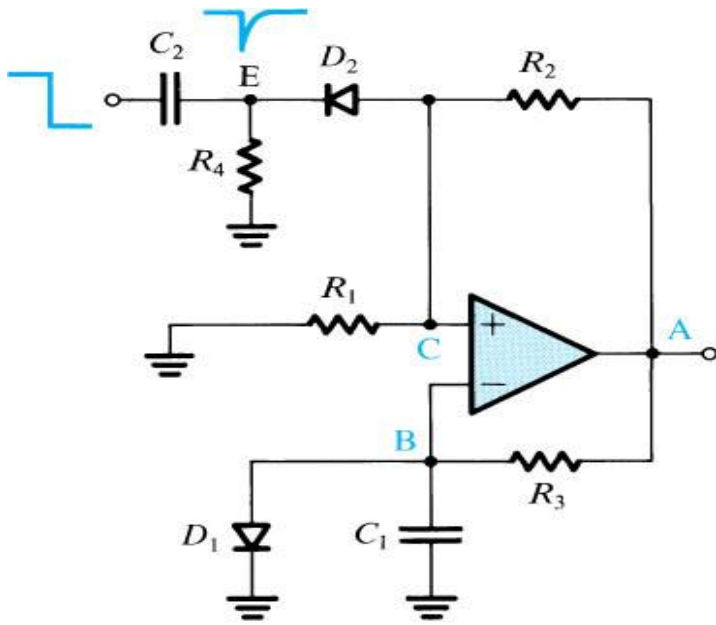
# Generation of a Standard Pulse

In the stable state,  $V_A=L+$  (why?),  $V_B=V_{D1}$ ,  $V_C=\beta L+$  (D2: ON and  $R4 \gg R1$ ).  
When a negative-going step applies at the trigger input:

- ➊ D2 conducts heavily and pulls node C down (lower than  $V_B$ ).
- ➋ The output of the op amp switch to L- and cause  $V_C$  to go toward  $\beta L-$ .
- ➌ D2 OFF and isolates the circuit from changes at the trigger input.
- ➍ D1 OFF and C1 begins to discharge toward L-.
- ➎ When  $V_B < V_C$ , the output of the op amp switch to L+.



# Generation of a Standard Pulse



$$v_B(t) = L_- - (L_- - V_{D1})e^{-t/R_3C_1}$$

$$v_B(T) = L_- - (L_- - V_{D1})e^{-T/R_3C_1} = \beta \cdot L_-$$

$$\rightarrow T \approx C_1R_3 \ln\left(\frac{V_{D1} - L_-}{\beta \cdot L_- - L_-}\right) \approx C_1R_3 \ln\left(\frac{1}{1-\beta}\right)$$

# The 555 Circuit

Commercially available integrated-circuit package such as 555 timer exists that contain the bulk of the circuitry needed to implement monostable and astable multivibrator.

